

# Project #2 Second Order ODE Applications

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This report involves modelling vibration of a spring-mass-damper mechanical system through manipulation of one-dimensional motion of mass differential equation (1).

$$(1) \quad mx'' + cx' + kx = F(t)$$

## Part A

Converting the mass motion differential equation (1) into an equation in terms of natural frequency and damping ratio.

$$\begin{aligned} \omega_n &= \sqrt{\frac{k}{m}} - \text{natural frequency vibration without damping} & x(0) &= x_0 \\ \zeta &= \frac{c}{2m\omega_n} - \text{damping ratio, indicates transient system response} & x'(0) &= x'_0 \end{aligned}$$

$$(2) \quad \begin{aligned} x'' + \frac{c}{m}x' + \frac{k}{m}x &= \frac{F(t)}{m}, & \frac{k}{m} &= \omega_n^2 \\ x'' + \frac{c}{m}x' + \omega_n^2x &= \frac{F(t)}{m}, & \frac{c}{m} &= 2\zeta\omega_n \\ \mathbf{x}'' + 2\zeta\omega_n\mathbf{x}' + \omega_n^2\mathbf{x} &= \frac{\mathbf{F}(t)}{\mathbf{m}} \end{aligned}$$

## Part B

$$\begin{aligned} x'' + 2\zeta\omega_nx' + \omega_n^2x &= \frac{F(t)}{m} & F(t) &= F_0\sin(\Omega t) & \Omega &- \text{frequency of forcing function} \\ x'' + 2\zeta\omega_nx' + \omega_n^2x &= \frac{F_0}{m}\sin(\Omega t) & x(0) &= x'(0) = 0 \end{aligned}$$

$$(3) \quad \therefore x(t) = x_c + x_p$$

$x_c$  - transient solution, homogeneous, reaches equilibrium due to damping  
 $x_p$  - steady state solution

Steady State Solution

$$(4) \quad x_c = e^{-\zeta\omega_n t} \left( A\cos(\sqrt{1-\zeta^2}\omega_n t) + B\sin(\sqrt{1-\zeta^2}\omega_n t) \right)$$

Solve for steady state - assume solution form

(5)

$$\begin{aligned}
 x_p &= A\cos(\Omega t) + B\sin(\Omega t) \\
 &\text{- assume } \Omega \neq \omega_n \\
 &\text{- sub } x_p(3) \text{ into ODE(1)} \\
 x_p' &= -\Omega A\sin(\Omega t) + \Omega B\cos(\Omega t) \\
 &= \Omega(-A\sin(\Omega t) + B\cos(\Omega t)) \\
 x_p'' &= \Omega(-\Omega A\cos(\Omega t) - \Omega B\sin(\Omega t)) \\
 &= -\Omega^2(A\cos(\Omega t) + B\sin(\Omega t))
 \end{aligned}$$

$$-\Omega^2(A\cos(\Omega t) + B\sin(\Omega t)) + 2\zeta\omega_n\Omega(-A\sin(\Omega t) + B\cos(\Omega t)) + \omega_n^2(A\cos(\Omega t) + B\sin(\Omega t)) = \frac{F_0}{m}\sin(\Omega t)$$

- collect likes and split into sine and cosine components

$$\begin{aligned}
 (6) \quad &-\Omega^2 B\sin(\Omega t) - 2\zeta\omega_n\Omega A\sin(\Omega t) + \omega_n^2 B\sin(\Omega t) = \frac{F_0}{m}\sin(\Omega t) \\
 &(B(\omega_n^2 - \Omega^2) - 2\zeta\omega_n\Omega A)\sin(\Omega t) = \frac{F_0}{m}\sin(\Omega t)
 \end{aligned}$$

$$\begin{aligned}
 (7) \quad &-\Omega^2 A\cos(\Omega t) + 2\zeta\omega_n\Omega B\cos(\Omega t) + \omega_n^2 A\cos(\Omega t) = \frac{F_0}{m}\sin(\Omega t) \\
 &(A(\omega_n^2 - \Omega^2) + 2\zeta\omega_n\Omega B)\cos(\Omega t) = 0
 \end{aligned}$$

- rearrange cosine (7) to solve for A

$$(8) \quad A = \frac{-2\zeta\omega_n\Omega B}{(\omega_n^2 - \Omega^2)}$$

- sub (8) into (6) to solve for B

$$\begin{aligned}
 (9) \quad &B(\omega_n^2 - \Omega^2) - 2\zeta\omega_n\Omega \frac{(-2\zeta\omega_n\Omega B)}{(\omega_n^2 - \Omega^2)} = \frac{F_0}{m} \\
 &\frac{B[(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2]}{(\omega_n^2 - \Omega^2)} = \frac{F_0}{m} \\
 \mathbf{B} &= \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2}
 \end{aligned}$$

- use solution of B (9) to solve for A (8)

$$\begin{aligned}
 (10) \quad \therefore A &= \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)(-2\zeta\omega_n\Omega)}{[(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2](\omega_n^2 - \Omega^2)} \\
 \mathbf{A} &= \frac{\frac{F_0}{m}(-2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2}
 \end{aligned}$$

$$(11) \quad \therefore \mathbf{x_p} = \frac{\frac{F_0}{m}(-2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2}\cos(\Omega t) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2}\sin(\Omega t)$$

- sub  $x_p$  (11) and  $x_c$  (4) into (3) and solve for A & B using initial conditions

$$\begin{aligned}
x(t) &= e^{-\zeta\omega_n t} A \cos(\sqrt{1-\zeta^2}\omega_n t) + e^{-\zeta\omega_n t} B \sin(\sqrt{1-\zeta^2}\omega_n t) + \\
&\quad \frac{\frac{F_0}{m}(-2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \cos(\Omega t) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \sin(\Omega t) \\
(12) \quad x(t) &= 0 \\
0 &= e^{-\zeta\omega_n(0)} A(1) + \frac{\frac{F_0}{m}(-2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} (1) \\
\mathbf{A} &= \frac{\frac{F_0}{m}(2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2}
\end{aligned}$$

$$\begin{aligned}
x'(t) &= 0 \\
x'(t) &= -\zeta\omega_n e^{-\zeta\omega_n t} A \cos(\sqrt{1-\zeta^2}\omega_n t) - e^{-\zeta\omega_n t} A(\sqrt{1-\zeta^2}\omega_n) \sin(\sqrt{1-\zeta^2}\omega_n t) - \\
&\quad \zeta\omega_n e^{-\zeta\omega_n t} B \sin(\sqrt{1-\zeta^2}\omega_n t) + e^{-\zeta\omega_n t} B(\sqrt{1-\zeta^2}\omega_n) \cos(\sqrt{1-\zeta^2}\omega_n t) + \\
&\quad \frac{\frac{F_0}{m}(2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \Omega \sin(\Omega t) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \Omega \cos(\Omega t) \\
(13) \quad 0 &= -\zeta\omega_n(1)A(1) + (1)B(\sqrt{1-\zeta^2}\omega_n)(1) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} (1) \\
0 &= -\zeta\omega_n \frac{\frac{F_0}{m}(2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} + B(\sqrt{1-\zeta^2}\omega_n) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)\Omega}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \\
\mathbf{B} &= \frac{\frac{F_0}{m}\Omega}{\sqrt{1-\zeta^2}\omega_n} \left[ \frac{(2\zeta^2\omega_n^2) + \Omega^2 - \omega_n^2}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \right]
\end{aligned}$$

- substituting A & B back into the x(t) (3) to achieve the final equation for displacement of the system

$$\begin{aligned}
\mathbf{x}(t) &= e^{-\zeta\omega_n t} \left[ \frac{\frac{F_0}{m}(2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \right] \cos(\sqrt{1-\zeta^2}\omega_n t) + \\
(14) \quad &e^{-\zeta\omega_n t} \frac{\frac{F_0}{m}\Omega}{\sqrt{1-\zeta^2}\omega_n} \left[ \frac{2\zeta^2\omega_n^2 + \Omega^2 - \omega_n^2}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \right] \sin(\sqrt{1-\zeta^2}\omega_n t) + \\
&\frac{\frac{F_0}{m}(-2\zeta\omega_n\Omega)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \cos(\Omega t) + \frac{\frac{F_0}{m}(\omega_n^2 - \Omega^2)}{(\omega_n^2 - \Omega^2)^2 + (2\zeta\omega_n\Omega)^2} \sin(\Omega t)
\end{aligned}$$

## Part C

MATLAB is used to solve the ODE (1) from Part A for the following constant values:

$$\left(\frac{F_0}{m}\right) = 1 \quad \omega_n = 1 \quad \zeta = 0.4 \quad \Omega = [0.1, 0.5, 1, 2, 10]$$

Figure 1 demonstrates maximum displacement behaviour of the mass-damper system (from rest) at the resonance frequency. This occurs as a result of forcing function constructively interfering with the spring's natural frequency following the direction of movement for the full period. Damping controls the maximum displacement value and controls the constant max amplitude, since without damping the amplitude of oscillations (displacement) of the mass would increase with time. The forcing functions with frequencies close to the resonance frequency show large displacement values, i.e  $\Omega = 0.5$ . However the further away from natural frequency the lower the displacement values of the mass-damper system. These frequencies represent the destructive interference of the forcing function against the spring's movement.

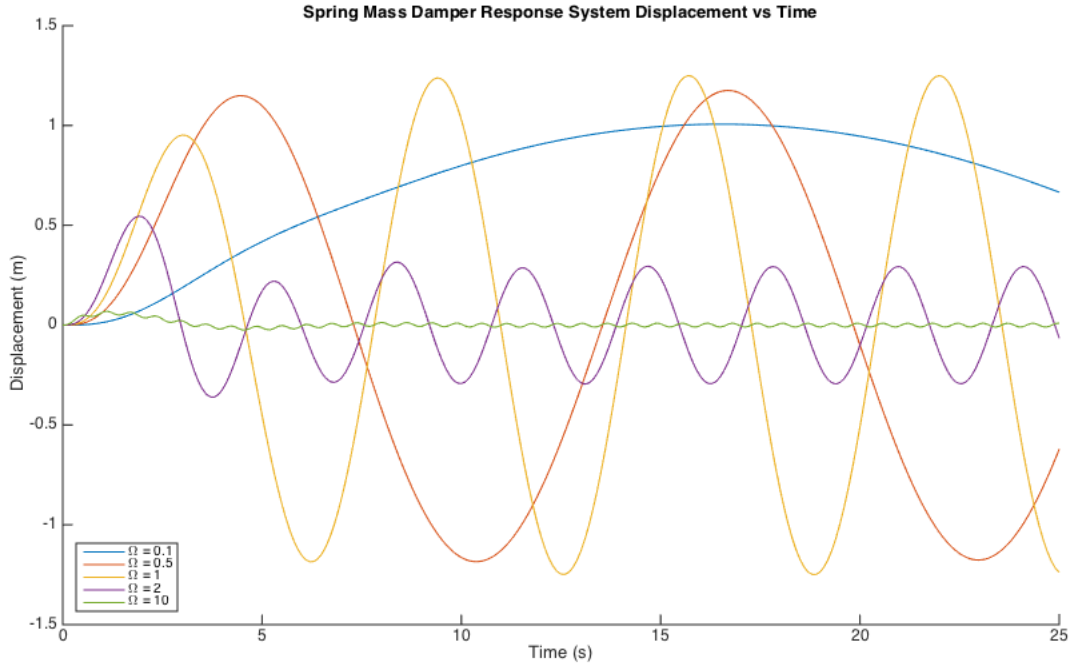


Figure 1: Overall response of the system for 5 values of forcing function frequency.

## Part D

Consider a simple spring mass system equation with a periodic forcing function based on Dirac delta function.

$$(15) \quad x'' + \omega_n^2 x = \frac{F_0}{m} \sum_{n=1}^{\infty} \delta(t - nT) \quad x(0) = x'(0) = 0$$

- use Laplace Transform to solve for displacement

$$(16) \quad \begin{aligned} \mathcal{L}\{x'' + \omega_n^2 x\} &= \mathcal{L}\left\{\frac{F_0}{m} \sum_{n=1}^{\infty} \delta(t - nT)\right\} \\ \mathcal{L}\{x''\} + \omega_n^2 X(s) &= \frac{F_0}{m} \sum_{n=1}^{\infty} e^{-nTs} \\ s^2 X(s) - sx(0) - x'(0) + \omega_n^2 X(s) &= \frac{F_0}{m} \sum_{n=1}^{\infty} e^{-nTs} \\ X(s)(s^2 + \omega_n^2) &= \frac{F_0}{m} \sum_{n=1}^{\infty} e^{-nTs} \\ X(s) &= \frac{\frac{F_0}{m} \sum_{n=1}^{\infty} e^{-nTs}}{(s^2 + \omega_n^2)} \end{aligned}$$

- take the inverse Laplace Transform

$$\begin{aligned}
(17) \quad \mathcal{L}^{-1}\{X(s)\} &= \mathcal{L}^{-1}\left\{\frac{\frac{F_0}{m} \sum_{n=1}^{\infty} e^{-nTs}}{(s^2 + \omega_n^2)}\right\} \\
x(t) &= \frac{F_0}{m} \sum_{n=1}^{\infty} \mathcal{L}^{-1}\left\{\frac{e^{-nTs}}{\omega_n} \bullet \frac{\omega_n}{(s^2 + \omega_n^2)}\right\} \\
\mathbf{x}(t) &= \frac{\mathbf{F}_0}{\omega_n \mathbf{m}} \sum_{n=1}^{\infty} [\sin(\omega_n(t - nT)) \bullet \mathbf{H}(t - nT)]
\end{aligned}$$

## Part E

MATLAB is used to plot the function (17) from Part D for the following constant values:

$$\left(\frac{F_0}{m}\right) = 1 \quad \omega_n = 1$$

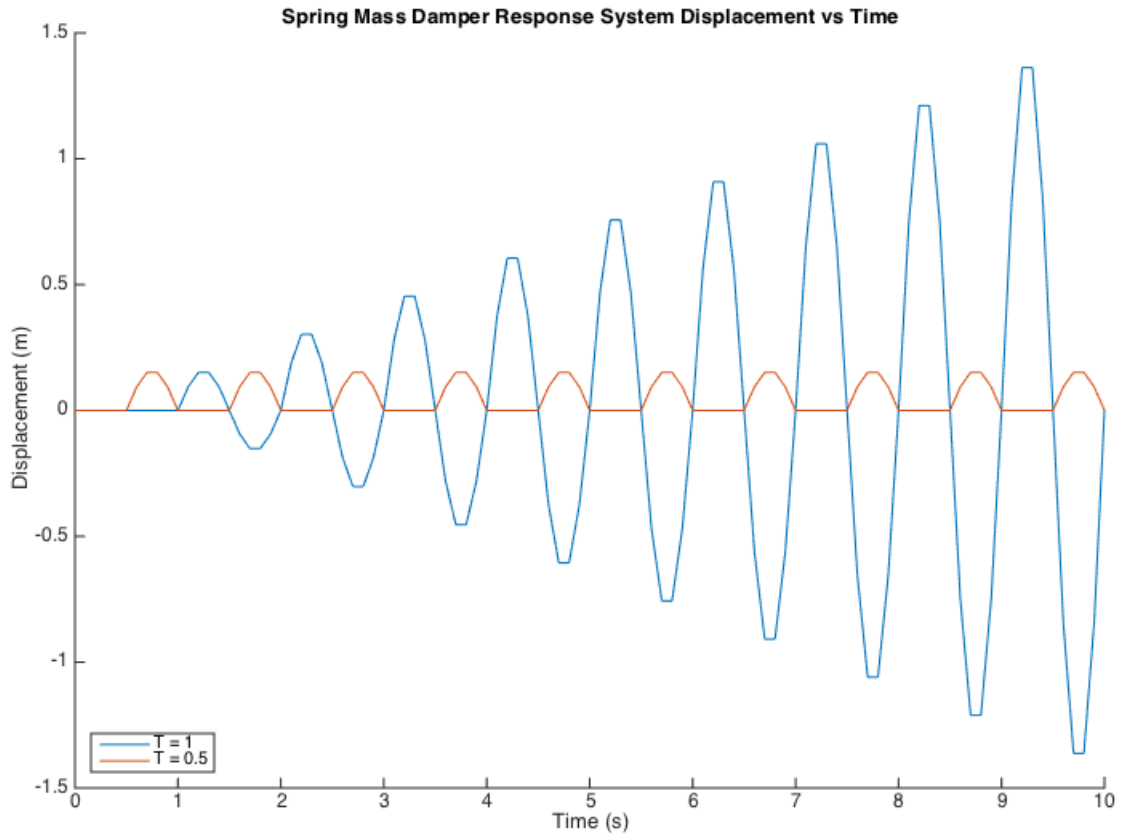


Figure 2: Overall response of the system when  $T = 1$  such that the frequency of the pings  $= \omega_n$ , and when  $T = 0.5$  such that the frequency of pings  $= 2\omega_n$ .

Figure 2 shows the constant increasing amplitude of displacement for ( $T = 1$ ) the system as the period forcing function matches the natural frequency of the spring and constructively interferes with the mass's movement. Since the system does not contain damping, the amplitude of displacement continues to increase with each period of oscillation. However pings occur at twice the natural frequency, for period forcing function is consistently destructively interfering with the system movement as it sets a max allowable amplitude and returns the system to rest, not allowing displacement in the downward direction.

## Appendix

### Part C MATLAB Script

```
1 clear all;
2 % Denifition of Variables
3 F0 = 1;
4 m = 1;
5 Wn = 1;
6 Z = 0.4;
7 Omega = [0.1, 0.5, 1, 2, 10];
8
9 %solving the differential equation of mass-spring-damper system with
10 %different omega values
11 for i = 1:5
12     syms x(t)
13     Dx = diff(x);
14     x(t) = dsolve(diff(x,2) + (2*Wn)*(Z*Dx) + (Wn^2)*x == (F0/m)*sin(Omega(i)*
15         t),...,
16         x(0)==0, Dx(0)==0)
17     %plotting spring-mass-damper system response
18     figure(1)
19     set(gca, 'FontSize', 12);
20     plot(0:0.1:25, x(0:0.1:25));
21     hold on
22     clear x(t)
23 end
24 %labeling the graph
25 title('Spring Mass Damper Response System Displacement vs Time')
26 ylabel('Displacement (m)')
27 xlabel('Time (s)')
28 legend('\Omega = 0.1', '\Omega = 0.5', '\Omega = 1', '\Omega = 2', '\Omega = 10', '
29     Location', 'southwest')
30 box off
```

### Part E MATLAB Script

```
1 clear all;
2 % Denifition of Variables
3 F0 = 1;
4 m = 1;
5 Wn = 2*pi;
6 T = [1, 0.5];
7
8 %plotting the Equation from Part D with different periods
9 syms n;
10 for i = 1:2
11     syms x(t)
12     Dx = diff(x);
13     x(t) = F0/(m*Wn) * symsum(sin(Wn*(t-n*T(i)))*heaviside(t-n*T(i)), n, 1,
14         inf);
15     %plotting spring-mass-damper system response
16     figure(2)
17     set(gca, 'FontSize', 12);
```

```
17     plot(0:0.1:10,x(0:0.1:10));
18     hold on
19     clear x(t)
20 end
21
22 %labeling the graph
23 title('Spring Mass Damper Response System Displacement vs Time')
24 ylabel('Displacement (m)')
25 xlabel('Time (s)')
26 legend('T = 1', 'T = 0.5', 'Location', 'southwest')
27 box off
```